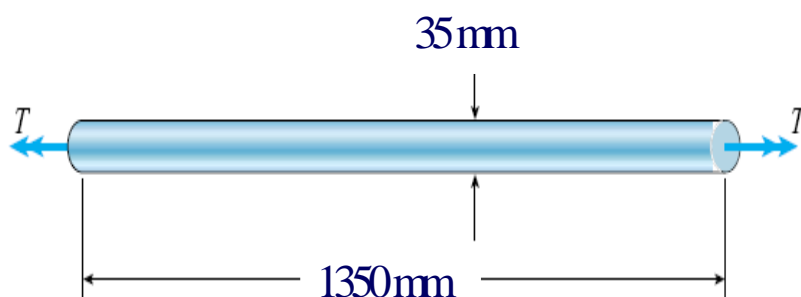


Primjer 4.1

Puni štap kružnog poprečnog presjeka, prečnika 40 mm, dužine 1350 mm i modula klizanja 80 GPa, opterećen je momentom uvijanja na svojim krajevima, kao što je dato na slici. Odrediti:

- Maksimalan tangencijalni napon u šipki, te ugao uvijanja ako je moment uvijanja 340 Nm
- Maksimalan mogući moment uvijanja, ako je dozvoljeni tangencijalni napon 4 MPa, a maksimalni dozvoljeni ugao uvijanja 2.5 stepeni



$$L := 1350 \text{ mm}$$

$$T := 340 \text{ N}\cdot\text{m}$$

$$D := 40 \text{ mm}$$

$$\tau_{\text{doz}} := 40 \text{ MPa}$$

$$G := 80 \text{ GPa}$$

$$\varphi_{\text{doz}} := 2.5^\circ$$

a)

$$\tau_{\text{max}} = \frac{T}{W_o} = \frac{16T}{D^3 \pi}$$

$$\tau_{\text{max}} := \frac{16T}{D^3 \pi} = 27.056 \text{ MPa}$$

$$\varphi = \frac{T \cdot L}{G \cdot I_o} \quad I_o = \frac{D^4 \pi}{32}$$

$$\varphi := \frac{32T \cdot L}{G \cdot D^4 \pi} = 1.308^\circ$$

b)

$$T_{\max 1} := \frac{\tau_{\text{doz}} \cdot D^3 \cdot \pi}{16} = 502.655 \text{ N} \cdot \text{m}$$

$$T_{\max 2} := \frac{\varphi_{\text{doz}} \cdot G \cdot D^4 \pi}{32L} = 649.85 \text{ N} \cdot \text{m}$$

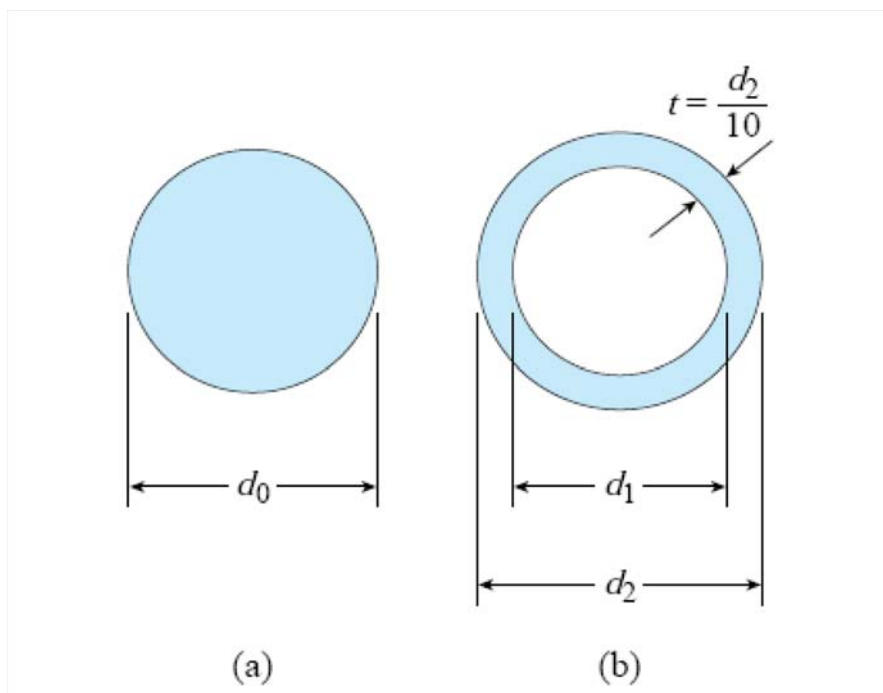
$$T_{\max} := \min(T_{\max 1}, T_{\max 2}) = 502.655 \text{ N} \cdot \text{m}$$

Primjer 4.2

Vratilo cilindričnog poprečnog presjeka od čelika, izrađeno u dvije varijante, kao puno i šuplje (slika), treba prenese moment uvijanja od 1200 Nm bez prekoračenja dozvoljenog tangencijalnog napona od 40MPa i dozvoljenog uzdužnog uvijanja od 0.75/m.

Treba odrediti:

- Prečnik punog vratila
- Potrebni vanjski prečnik šupljeg vratila ako je debljina stjenke vratila jedna desetina vanjskog prečnika
- Odnos prečnika (d_2/d_1) i težina oba vratila



$$T := 1200 \text{ N}\cdot\text{m}$$

$$E := 200 \text{ GPa} \quad \nu := 0.3$$

$$\tau_{\text{doz}} := 40 \text{ MPa}$$

$$G := \frac{E}{2 \cdot (1 + \nu)} = 76.923 \text{ GPa}$$

$$\theta_{\text{doz}} := 0.75 \frac{\circ}{\text{m}}$$

a) puno vratilo

$$\tau_{\text{doz}} = \frac{T}{W_o} = \frac{16T}{d_0^3 \pi}$$

$$d_{01} := \sqrt[3]{\frac{16T}{\tau_{\text{doz}} \cdot \pi}} = 53.46 \text{ mm}$$

$$\theta_{\text{doz}} = \frac{T}{G \cdot I_o} \quad I_o = \frac{d_0^4 \pi}{32}$$

$$d_{02} := \sqrt[4]{\frac{32T}{G \cdot \pi \cdot \theta_{\text{doz}}}} = 59.026 \text{ mm}$$

$$d_0 := \max(d_{01}, d_{02}) = 59.026 \text{ mm}$$

b) šuplje vratilo

$$d_1 = d_2 - 2t = 0.8d_2$$

$$I_o = (d_2^4 - d_1^4) \cdot \frac{\pi}{32} = (1 - 0.8^4) \cdot \frac{\pi}{32} d_2^4$$

$$\tau_{\text{doz}} = \frac{T \cdot \frac{d_2}{2}}{I_o} = \frac{T}{(1 - 0.8^4) \cdot \frac{\pi}{16} \cdot d_2^3}$$

$$d_{21} := \sqrt[3]{\frac{16T}{\tau_{\text{doz}} \cdot \pi \cdot (1 - 0.8^4)}} = 63.726 \text{ mm}$$

$$\theta_{\text{doz}} = \frac{T}{G \cdot I_0}$$

$$d_{22} := \sqrt[4]{\frac{32T}{G \cdot \pi \cdot (1 - 0.8^4) \cdot \theta_{\text{doz}}}} = 67.338 \text{ mm}$$

$$d_2 := \max(d_{21}, d_{22}) = 67.338 \text{ mm}$$

$$d_1 := 0.8d_2 = 53.87 \text{ mm}$$

c) Odnos prečnika i težina

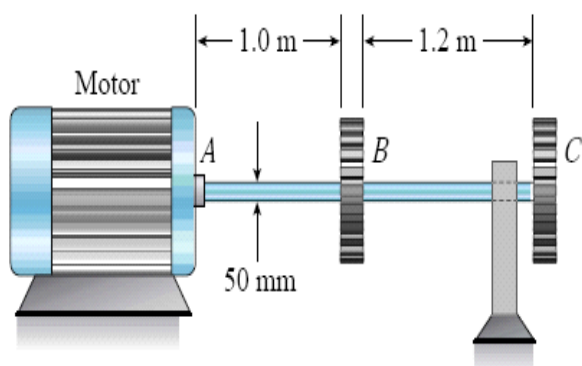
$$\frac{d_2}{d_0} = 1.141$$

$$\frac{W_{\text{šuplje}}}{W_{\text{puno}}} = \frac{\gamma \cdot V_{\text{šuplje}}}{\gamma \cdot V_{\text{puno}}} = \frac{A_{\text{šuplje}}}{A_{\text{puno}}} = \frac{(d_2^2 - d_1^2) \cdot \frac{\pi}{4}}{d_0^2 \cdot \frac{\pi}{4}}$$

$$\frac{(d_2^2 - d_1^2)}{d_0^2} = 0.469$$

Primjer 4.3

Puno vratilo ABC prečnika 50 mm se pokreće motorom snage 50 kW i frekvencije 10 Hz u tački A . Zupčanici B i C pokreću uređaje koji potražuju snagu od 35 i 15 kW, respektivno. Odrediti najveći tangencijalni napon τ_{\max} u vratilu i ugao uvijanja ϕ_{AC} između motora A i zupčanika C . Uzeti da je $G=80$ Gpa.



$$P := 50\text{kW}$$

$$G := 80\text{GPa}$$

$$P_B := 35\text{kW}$$

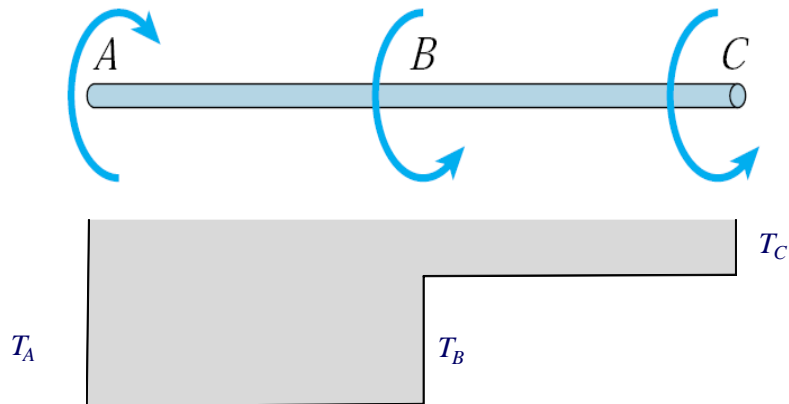
$$f := 10\text{Hz}$$

$$P_C := 15\text{kW}$$

$$d := 50\text{mm}$$

$$L_{AB} := 1000\text{mm}$$

$$L_{BC} := 1200\text{mm}$$



$$T_A := \frac{P}{2\pi \cdot f} = 795.775 \cdot \text{N} \cdot \text{m}$$

$$T_B := \frac{P_B}{2\pi \cdot f} = 557.042 \cdot \text{N} \cdot \text{m}$$

$$T_C := \frac{P_C}{2\pi \cdot f} = 238.732 \cdot \text{N} \cdot \text{m}$$

$$T_{AB} := T_A = 795.775 \cdot \text{N} \cdot \text{m}$$

$$T_{BC} := T_C = 238.732 \cdot \text{N} \cdot \text{m}$$

$$I_0 := \frac{d^4 \cdot \pi}{32}$$

$$\tau_{AB} := \frac{T_{AB}}{\left(\frac{d^3 \pi}{16} \right)} = 32.423 \cdot \text{MPa}$$

$$\phi_{AB} := \frac{T_{AB} \cdot L_{AB}}{G \cdot I_0} = 0.016$$

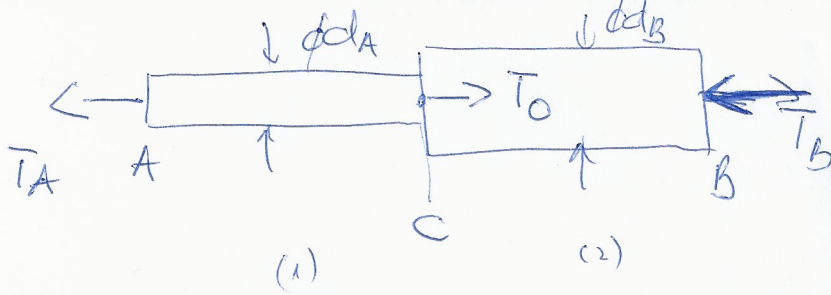
$$\tau_{BC} := \frac{T_{BC}}{\left(\frac{d^3 \pi}{16} \right)} = 9.727 \cdot \text{MPa}$$

$$\phi_{BC} := \frac{T_{BC} \cdot L_{BC}}{G \cdot I_0} = 5.836 \times 10^{-3}$$

$$\tau_{\max} := \max(\tau_{AB}, \tau_{BC}) = 32.423 \cdot \text{MPa}$$

$$\phi_{AC} := \phi_{AB} + \phi_{BC} = 0.022$$

$$\phi_{AC} = 1.263 \cdot ^\circ$$



Jednačine ravnoteže

$$\bar{T}_A + \bar{T}_B = \bar{T}_0 \quad (1)$$

Jednačine kompatibilnosti

$$\psi_1 + \psi_2 = 0 \quad (2)$$

ili

superpozicija

$$\psi_{T_0} = \psi_{T_B} \quad (3)$$

$$\psi_{T_0} = \frac{T_0 L_{AC}}{G I_{OAC}}$$

$$\psi_{T_B} = - \frac{T_B \cdot L_{AC}}{G I_{OAC}} - \frac{T_B \cdot L_{BC}}{G I_{OBC}} \quad (4)$$

$$(4) \rightarrow (3) \Rightarrow T_B = T_0 \frac{L_{AC} I_{OBC}}{L_{AC} I_{OBC} + L_{BC} I_{OAC}} \quad (5)$$

$$(5) \Rightarrow (1) \Rightarrow \bar{T}_A = T_0 \frac{L_{BC} I_{OAC}}{L_{AC} I_{OBC} + L_{BC} I_{OAC}} \quad (6)$$

$$\bar{T}_{AC} = \frac{\bar{T}_A d_A}{2 I_{OAC}} \quad \bar{T}_{BC} = \frac{\bar{T}_B d_B}{2 I_{OBC}} \quad (7)$$

$$(5); (6) \Rightarrow (7)$$

$$\tilde{\tau}_{AC} = \frac{\tilde{T}_0 L_{BC} d_A}{2(L_{AC} l_{BC} + L_{BC} l_{AC})}$$

$$\tilde{\tau}_{BC} = \frac{\tilde{T}_0 L_{AC} d_B}{2(L_{AC} l_{BC} + L_{BC} l_{AC})}$$

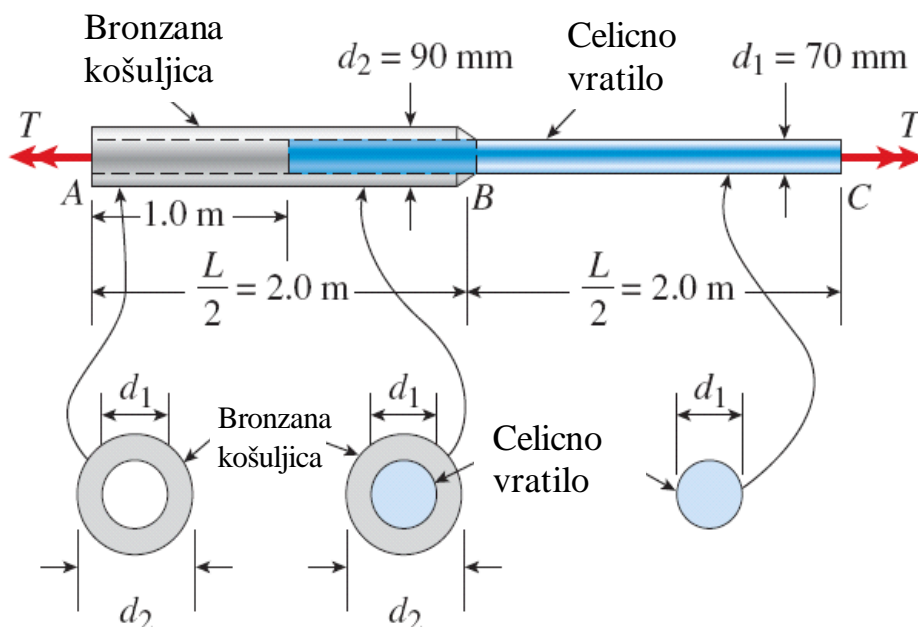
$$\max \tilde{\tau} = \max(\tilde{\tau}_{AC}, \tilde{\tau}_{BC}) = \max(L_{BC} \cdot d_A, L_{AC} d_B)$$

$$\rho_C = \frac{\tilde{T}_A \cdot L_{AC}}{G \cdot l_{AC}} = \frac{\tilde{T}_B \cdot L_{BC}}{G \cdot l_{BC}} = \tilde{T}_0 \frac{L_{AC} L_{BC}}{G(L_{AC} l_{BC} + L_{BC} l_{AC})}$$

Primjer 4.5

Vratilo izrađeno od čelika ($G_c=80$ GPa), dužine 3 m, je trećinom dužine uvučeno u bronzanu košuljicu ($G_b=40$ GPa) koja je čvrsto povezana s vratilom. Vanjski prečnici vratila i košuljice su $d_1=70$ mm i $d_2=90$ mm, respektivno. Odrediti:

- Dozvoljeni moment uvijanja T_1 koji se može primijeniti na krajeve ako je dozvoljeni napon uvijanja između krajeva 8 stepeni.
- Dozvoljeni moment uvijanja T_2 ako je dozvoljni tangencijalni napon bronzne $\tau_b=70$ Mpa
- Dozvoljeni moment uvijanja T_3 ako je dozvoljni tangencijalni napon čelika $\tau_c=110$ Mpa
- Dozvoljeni moment uvijanja T_{max} ako moraju biti zadovoljena sva tri uslova pod a), b), c)



$$\begin{array}{lll}
 L_1 := 1\text{m} & G_{\check{c}} := 80\text{GPa} & \phi_{\text{doza}} := 8^\circ \\
 L_2 := 1\text{m} & G_b := 40\text{GPa} & \tau_{\text{dozb}} := 70\text{MPa} \\
 L_3 := 2\text{m} & & \tau_{\text{dozc}} := 110\text{MPa} \\
 d_1 := 70\text{mm} & & \\
 d_2 := 90\text{mm} & &
 \end{array}$$

a)

$$I_{0\check{c}} := \frac{d_1^4 \cdot \pi}{32} = 2.357 \times 10^6 \text{mm}^4$$

$$I_{0b} := \frac{(d_2^4 - d_1^4) \cdot \pi}{32} = 4.084 \times 10^6 \text{mm}^4$$

$$\phi_a = \frac{T_1 \cdot L_1}{G_b \cdot I_{0b}} + \frac{T_{\check{c}} \cdot L_2}{G_{\check{c}} \cdot I_{0\check{c}}} + \frac{T_1 \cdot L_3}{G_{\check{c}} \cdot I_{0\check{c}}}$$

$$T_{\check{c}} = T_1 \cdot \frac{G_{\check{c}} \cdot I_{0\check{c}}}{G_{\check{c}} \cdot I_{0\check{c}} + G_b \cdot I_{0b}}$$

$$\phi_a = \frac{T_1 \cdot L_1}{G_b \cdot I_{0b}} + \frac{L_2}{G_{\check{c}} \cdot I_{0\check{c}}} \cdot \left(T_1 \cdot \frac{G_{\check{c}} \cdot I_{0\check{c}}}{G_{\check{c}} \cdot I_{0\check{c}} + G_b \cdot I_{0b}} \right) + \frac{T_1 \cdot L_3}{G_{\check{c}} \cdot I_{0\check{c}}}$$

$$T_1 := \frac{\phi_{\text{doza}}}{\frac{L_2}{G_b \cdot I_{0b} + G_{\check{c}} \cdot I_{0\check{c}}} + \frac{L_3}{G_{\check{c}} \cdot I_{0\check{c}}} + \frac{L_1}{G_b \cdot I_{0b}}} = 7.135 \times 10^3 \text{N}\cdot\text{m}$$

b)

$$\tau_{\text{dozb}} = \frac{T_2 \cdot \frac{d_2}{2}}{I_{0b}} \quad T_{21} := \frac{2\tau_{\text{dozb}} \cdot I_{0b}}{d_2} = 6.353 \text{ kN}\cdot\text{m}$$

$$\tau_{\text{dozb}} = \frac{T_b \cdot \frac{d_2}{2}}{I_{0b}} \quad \tau_1 = T_2 \frac{G_b \cdot I_{0b}}{G_{\check{c}} \cdot I_{0\check{c}} + G_b \cdot I_{0b}} \cdot \frac{d_2}{2 \cdot I_{0b}}$$
$$T_b = T_2 \cdot \frac{G_b \cdot I_{0b}}{G_{\check{c}} \cdot I_{0\check{c}} + G_b \cdot I_{0b}}$$

$$T_{22} := \frac{2 \cdot \tau_{\text{dozb}} \cdot (G_b \cdot I_{0b} + G_{\check{c}} \cdot I_{0\check{c}})}{G_b \cdot d_2} = 13.686 \text{ kN}\cdot\text{m}$$

$$T_2 := \min(T_{21}, T_{22}) = 6.353 \text{ kN}\cdot\text{m}$$

c)

$$\tau_{\text{dozc}} = \frac{T_{\check{c}} \cdot \frac{d_2}{2}}{I_{0b}} \quad \tau_{\text{dozc}} = T_3 \frac{G_{\check{c}} \cdot I_{0\check{c}}}{G_{\check{c}} \cdot I_{0\check{c}} + G_b \cdot I_{0b}} \cdot \frac{d_1}{2 \cdot I_{0\check{c}}}$$
$$T_{\check{c}} = T_3 \cdot \frac{G_{\check{c}} \cdot I_{0\check{c}}}{G_{\check{c}} \cdot I_{0\check{c}} + G_b \cdot I_{0b}}$$

$$T_{31} := \frac{2 \cdot \tau_{\text{dozc}} \cdot (G_b \cdot I_{0b} + G_{\check{c}} \cdot I_{0\check{c}})}{d_1 \cdot G_{\check{c}}} = 13.826 \text{ kN}\cdot\text{m}$$

$$\tau_{\text{dozc}} = \frac{T_3 \cdot \frac{d_1}{2}}{I_{0\check{c}}} \quad T_{32} := \frac{2\tau_{\text{dozc}} \cdot I_{0\check{c}}}{d_1} = 7.408 \text{ kN}\cdot\text{m}$$

$$T_3 := \min(T_{31}, T_{32}) = 7.408 \text{ kN}\cdot\text{m}$$

d)

$$T_{\text{max}} := \min(T_1, T_2, T_3) = 6.353 \text{ kN}\cdot\text{m}$$