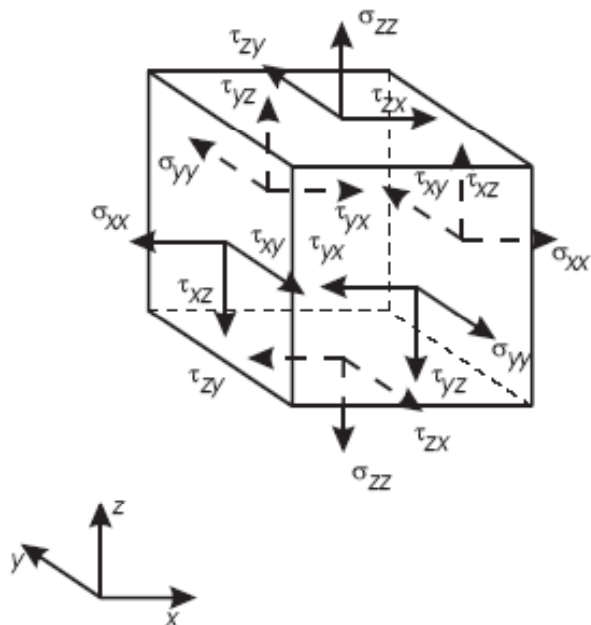


Naprezanje u dva pravca*

Opšte stanje napona

Tenzor napona

$$\begin{bmatrix} \sigma_{xx} & \tau_{xy} & \tau_{xz} \\ \tau_{yx} & \sigma_{yy} & \tau_{yz} \\ \tau_{zx} & \tau_{zy} & \sigma_{zz} \end{bmatrix} \quad \begin{bmatrix} \sigma_{xx} & \sigma_{xy} & \sigma_{xz} \\ \sigma_{yx} & \sigma_{yy} & \sigma_{yz} \\ \sigma_{zx} & \sigma_{zy} & \sigma_{zz} \end{bmatrix} \quad \begin{aligned} \tau_{xy} &= \tau_{yx} \\ \tau_{xz} &= \tau_{zx} \\ \tau_{yz} &= \tau_{zy} \end{aligned}$$



Značenje indeksa

Normalni napon: indeksi pokazuju površinu na koju djeluje.

Tangencijalni napon: prvi indeks pokazuje površinu na koju napon djeluje, a drugi pravac u kojem djeluje.

Konvencija o predznaku napona

Normalni napon je pozitivan ako se njegov smjer poklapa sa smjerom vanjske normale na elementu površine

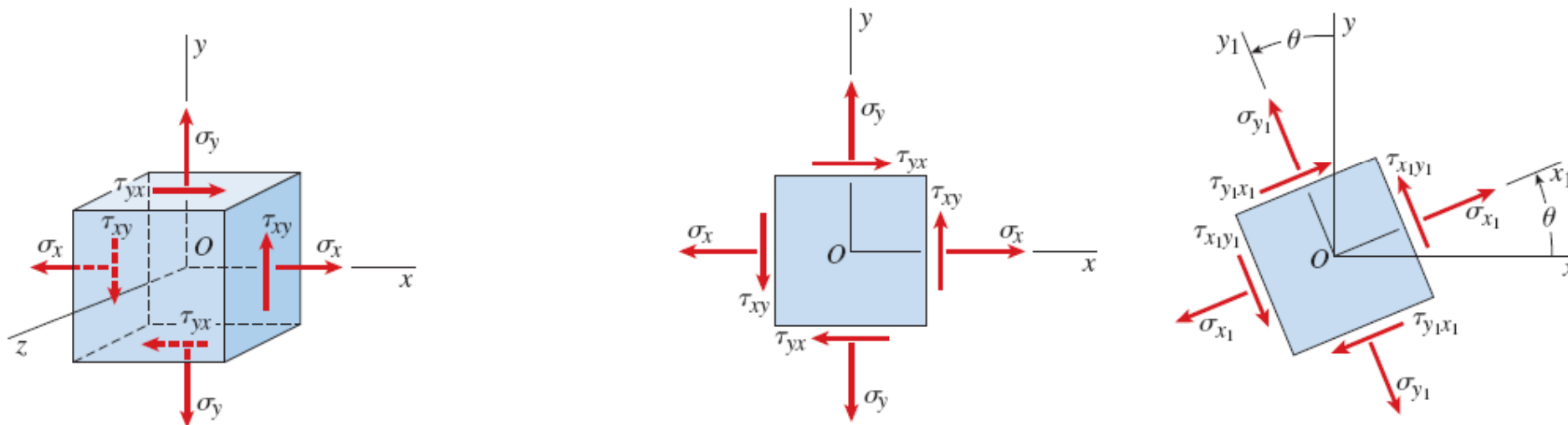
Tangencijalni napon je pozitivan ako je na gornjoj i desnoj površini elementa usmjeren ka pozitivnom smjeru ose.

*Grupa autora, *Elastostatika I*, Tehnički fakultet, Bihać, 2003

Naprezanje u dva pravca*

Ravno stanje napona

Ravno stanje napona – jedinstveno predstavljeno s dvije komponente normalnog napona i jednom komponentom tangencijalnog napona koji djeluju na element s određenim položajem u tački elementa.

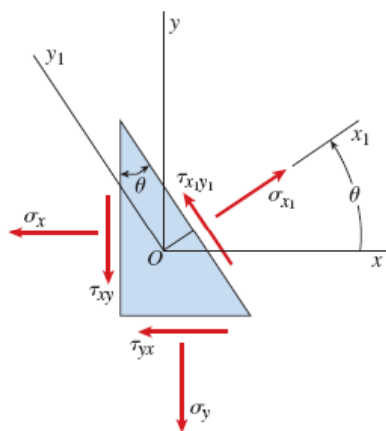


$$\tau_{xy} = \tau_{yx}$$

$$\tau_{x_1 y_1} = \tau_{y_1 x_1}$$

Naprezanje u dva pravca

Naponi na kosoj ravni



$$\sum_i F_{x_1 i} = 0$$

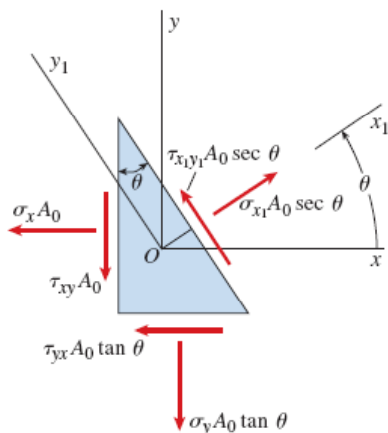
$$\sigma_{x_1} A_0 \sec(\theta) - \sigma_x A_0 \cos(\theta) - \tau_{xy} A_0 \sin(\theta) +$$

$$- \sigma_y A_0 \operatorname{tg}(\theta) \sin(\theta) - \tau_{yx} A_0 \operatorname{tg}(\theta) \cos(\theta) = 0 \quad (3.1)$$

$$\sum_i F_{y_1 i} = 0$$

$$\tau_{x_1 y_1} A_0 \sec(\theta) + \sigma_x A_0 \sin(\theta) - \tau_{xy} A_0 \cos(\theta) +$$

$$- \sigma_y A_0 \operatorname{tg}(\theta) \cos(\theta) + \tau_{yx} A_0 \operatorname{tg}(\theta) \sin(\theta) = 0 \quad (3.2)$$



$$\sigma_{x_1} = \sigma_x \cos^2(\theta) + \sigma_y \sin^2(\theta) + 2\tau_{yx} \sin(\theta) \cos(\theta) \quad (3.3)$$

$$\tau_{x_1 y_1} = -(\sigma_x - \sigma_y) \sin(\theta) \cos(\theta) + 2\tau_{yx} (\cos^2(\theta) - \sin^2(\theta)) \quad (3.4)$$

Naprežanje u dva pravca

Naponi na kosoj ravni

$$\sigma_{x_1} = \sigma_x \cos^2(\theta) + \sigma_y \sin^2(\theta) + 2\tau_{yx} \sin(\theta) \cos(\theta) \quad (3.3)$$

$$\tau_{x_1y_1} = -(\sigma_x - \sigma_y) \sin(\theta) \cos(\theta) + 2\tau_{yx} (\cos^2(\theta) - \sin^2(\theta)) \quad (3.4)$$

$$\cos^2(\theta) = \frac{1}{2}(1 + \cos(2\theta)) \quad \sin^2(\theta) = \frac{1}{2}(1 - \cos(2\theta)) \quad \sin(\theta) \cos(\theta) = \frac{1}{2} \sin(2\theta)$$

$$\sigma_{x_1} = \frac{\sigma_x + \sigma_y}{2} + \frac{\sigma_x - \sigma_y}{2} \cos(2\theta) + \tau_{xy} \sin(2\theta) \quad (3.5)$$

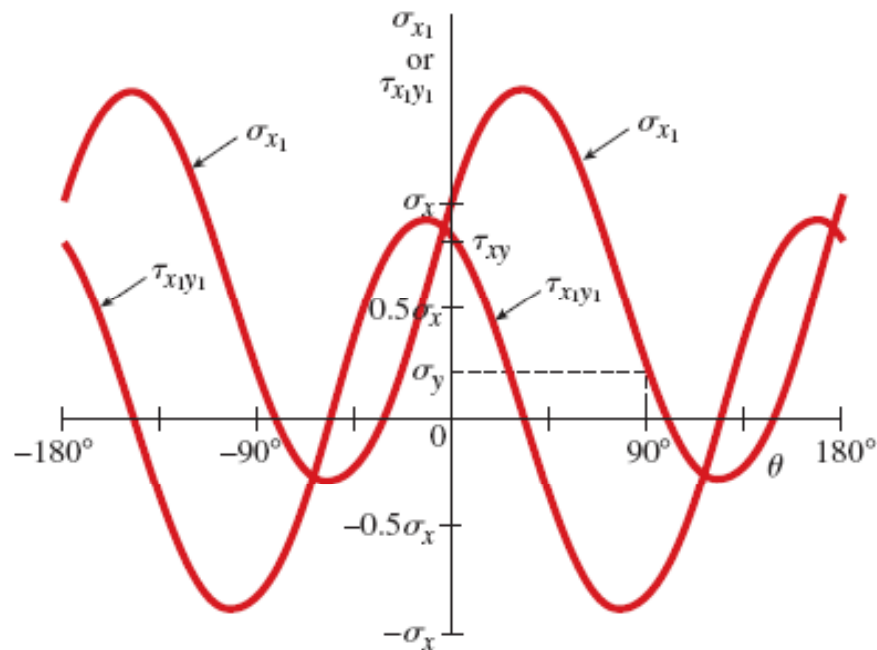
$$\tau_{x_1y_1} = -\frac{\sigma_x - \sigma_y}{2} \sin(2\theta) + \tau_{xy} \cos(2\theta) \quad (3.6)$$

Naprežanje u dva pravca

Naponi na kosoj ravni

$$\sigma_{x_1} = \frac{\sigma_x + \sigma_y}{2} - \frac{\sigma_x - \sigma_y}{2} \cos(2\theta) - \tau_{xy} \sin(2\theta) \quad (3.6)$$

$$\sigma_{x_1} + \sigma_{y_1} = \sigma_x + \sigma_y \quad (3.7)$$



Naprezanje u dva pravca

Glavni normalni naponi i najveći tangencijalni naponi

$$\sigma_{x_1} = \frac{\sigma_x + \sigma_y}{2} + \frac{\sigma_x - \sigma_y}{2} \cos(2\theta) + \tau_{xy} \sin(2\theta) \quad (3.5)$$

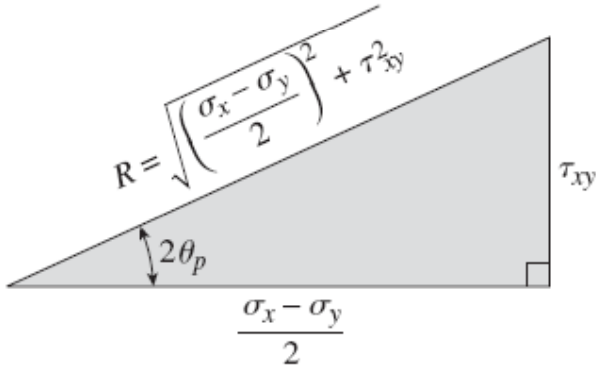
$$\left. \frac{d\sigma_{x_1}}{d\theta} \right|_{\theta=\alpha} = -(\sigma_x - \sigma_y) \sin(2\theta) + 2\tau_{xy} \cos(2\theta) \Big|_{\theta=\alpha} = 0 \quad (3.8)$$

$$(3.8) \quad \rightarrow \quad \operatorname{tg}(2\alpha) = \frac{2\tau_{xy}}{\sigma_x - \sigma_y} \quad (3.9)$$

- Ugao α određuje ravan maksimalnog/minimalnog normalnog napona
- Jednačina (3.9) ima dva korijena u domenu $(0, 2\pi)$, a oni ovise od predznaka τ_{xy} i $(\sigma_x - \sigma_y)$ – ovi korijeni se nazivaju i **uglovi glavnih ravni**

Naprezanje u dva pravca

Glavni normalni naponi i najveći tangencijalni naponi



$$R = \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$

$$\cos(2\alpha) = \frac{\sigma_x - \sigma_y}{2R}$$

$$\sin(2\alpha) = \frac{\tau_{xy}}{R}$$

$$\sigma_{x_1} = \frac{\sigma_x + \sigma_y}{2} + \frac{\sigma_x - \sigma_y}{2} \cos(2\theta) + \tau_{xy} \sin(2\theta) \quad (3.5)$$

$$\tau_{x_1y_1} = -\frac{\sigma_x - \sigma_y}{2} \sin(2\theta) + \tau_{xy} \cos(2\theta) \quad (3.6)$$

$$\sigma_{x_1} + \sigma_{y_1} = \sigma_x + \sigma_y = \sigma_1 + \sigma_2 \quad (3.7)$$

$$\sigma_1 = \frac{\sigma_x + \sigma_y}{2} + \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2} \quad (3.10)$$

$$\sigma_2 = \frac{\sigma_x + \sigma_y}{2} - \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2} \quad (3.11)$$

U ravni glavnih normalnih napona ne djeluju tangencijalni naponi, tj. $\tau_{12}=0$

Naprezanje u dva pravca

Glavni normalni naponi i najveći tangencijalni naponi

$$\tau_{x_1y_1} = -\frac{\sigma_x - \sigma_y}{2} \sin(2\theta) + \tau_{xy} \cos(2\theta) \quad (3.6)$$

$$\left. \frac{d\tau_{x_1y_1}}{d\theta} \right|_{\theta=\beta} = -(\sigma_x - \sigma_y) \cos(2\theta) - 2\tau_{xy} \sin(2\theta) \Big|_{\theta=\alpha} = 0 \quad (3.12)$$

$$(3.12) \quad \rightarrow \quad \operatorname{tg}(2\beta) = -\frac{\sigma_x - \sigma_y}{2\tau_{xy}} = \frac{1}{\operatorname{tg}(2\alpha)} \quad (3.13)$$

- Ugao β određuje ravan maksimalnog/minimalnog tangencijalnog napona
- Jednačina (3.13) ima dva korijena u domenu $(0, 2\pi)$, a oni ovise od predznaka τ_{xy} i $(\sigma_x - \sigma_y)$ – za ugao β prema (3.13) vrijedi

$$\beta = \alpha \pm 45^\circ$$

Naprezanje u dva pravca

Glavni normalni naponi i najveći tangencijalni naponi

$$\sigma_{x_1} = \frac{\sigma_x + \sigma_y}{2} + \frac{\sigma_x - \sigma_y}{2} \cos(2\theta) + \tau_{xy} \sin(2\theta) \quad (3.5)$$

$$\tau_{x_1y_1} = -\frac{\sigma_x - \sigma_y}{2} \sin(2\theta) + \tau_{xy} \cos(2\theta) \quad (3.6)$$

$$\sigma_{x_1} + \sigma_{y_1} = \sigma_x + \sigma_y = \sigma_1 + \sigma_2 \quad (3.7)$$

$$R = \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$

$$\cos(2\alpha) = \frac{\tau_{xy}}{2R}$$

$$\sin(2\alpha) = -\frac{\sigma_x - \sigma_y}{R}$$

$$\tau_{\max, \min} = \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2} = \pm \frac{\sigma_1 - \sigma_2}{2} \quad (3.14)$$

U ravni najvećih tangencijalnih napona djeluju normalni naponi

$$\sigma = \frac{\sigma_x + \sigma_y}{2} = \frac{\sigma_1 + \sigma_2}{2} \quad (3.15)$$

Naprezanje u dva pravca

Mohr-ov (Mor) krug napona

Jednačine za računanje napona mogu se predstaviti grafički pomoću *Mohr-ovog* kruga napona. Iz jednačina (3.5) i (3.6) se eliminiše ugao 2θ

$$\sigma_{x_1} = \frac{\sigma_x + \sigma_y}{2} + \frac{\sigma_x - \sigma_y}{2} \cos(2\theta) + \tau_{xy} \sin(2\theta) \quad (3.5)$$

$$\tau_{x_1y_1} = -\frac{\sigma_x - \sigma_y}{2} \sin(2\theta) + \tau_{xy} \cos(2\theta) \quad (3.6)$$

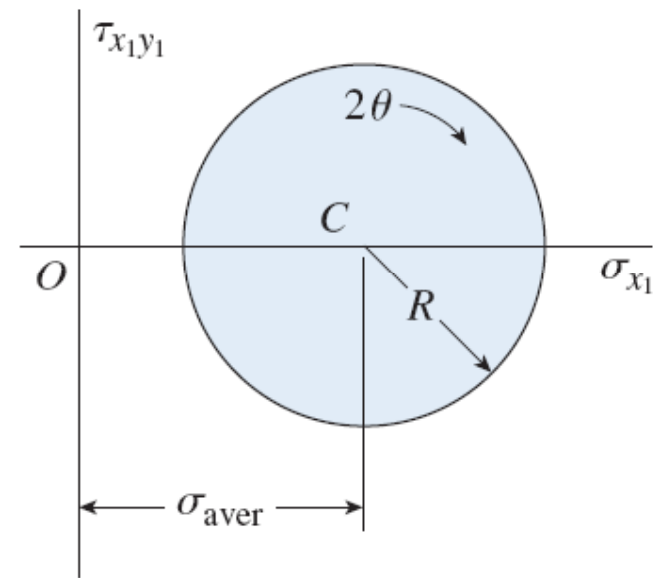
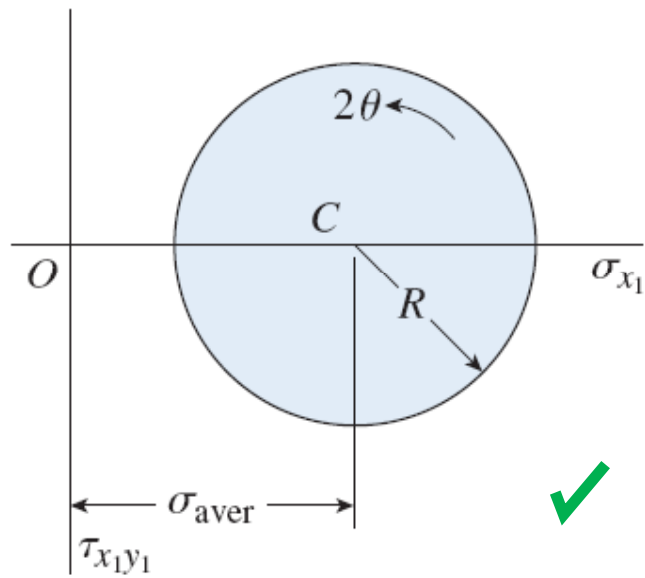
Jednačine za računanje napona mogu se predstaviti grafički pomoću *Mohr-ovog* kruga napona. Iz jednačina (3.5) i (3.6) se eliminiše ugao tako što se obje jednačine kvadriraju i sabere, pa se dobije:

$$\left(\sigma_{x_1} - \frac{\sigma_x + \sigma_y}{2} \right)^2 + \tau_{x_1y_1}^2 = \left(\frac{\sigma_x - \sigma_y}{2} \right)^2 + \tau_{xy}^2 \quad (3.16)$$

$$\left(\sigma_{x_1} - \sigma_{sr} \right)^2 + \tau_{x_1y_1}^2 = R^2 \quad (3.16a)$$

Naprezanje u dva pravca

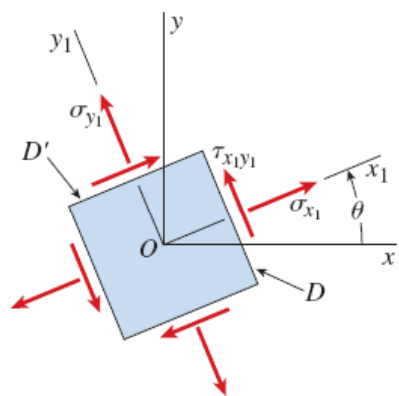
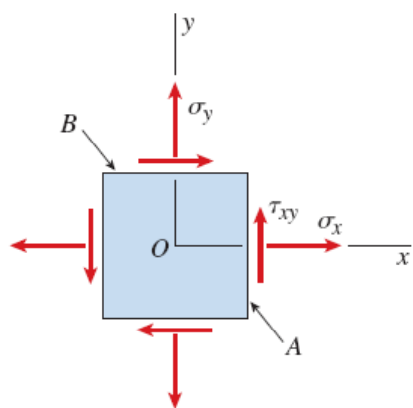
Mohr-ov (Mor) krug napona – konstrukcija



Dva načina crtanja *Mohr*-ovog kruga napona

Naprezanje u dva pravca

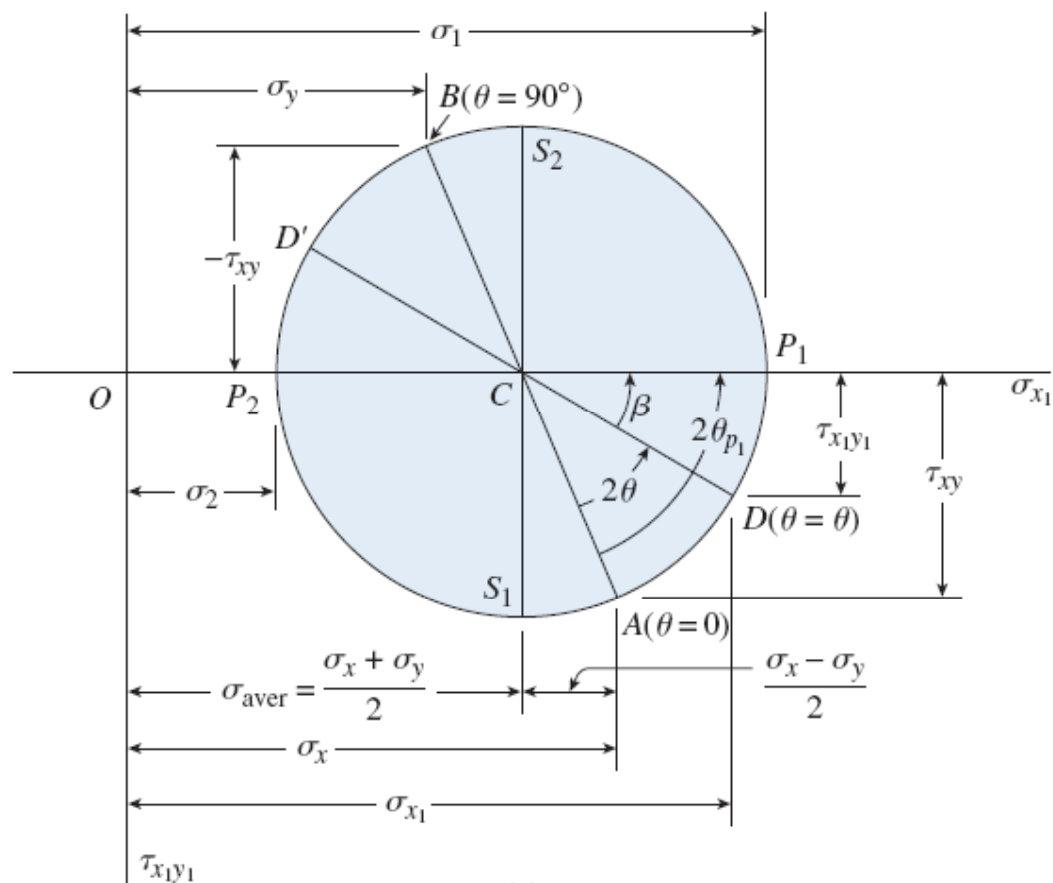
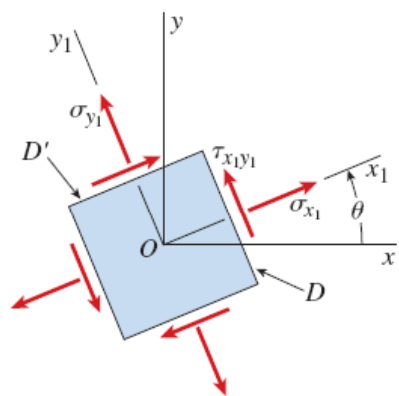
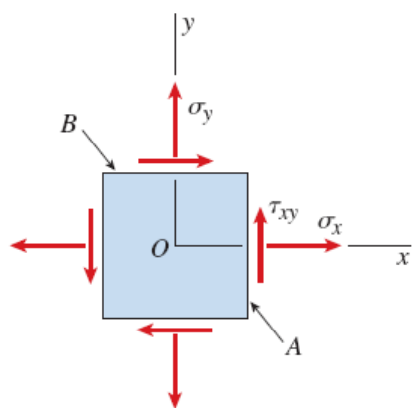
Mohr-ov (Mor) krug napona – konstrukcija



- Nacrta se koordinatni sistem s abscisom σ_{x_1} (σ_n), pozitivna na desno, i ordinatom τ_{xy} (τ_n), pozitivna na dole
- U dijagramu se ucrtava tačka A s koordinatama (σ_x, τ_{xy}) – predstavlja naponsko stanje na pozitivnoj x površi (površ A)
- U dijagramu se ucrtava tačka B s koordinatama $(\sigma_y, -\tau_{xy})$ – predstavlja naponsko stanje na pozitivnoj y površi (površ B)
- Povučete se duž od AB koja predstavlja prečnik kruga napona s centrom u tački C .
- Koristeći tačku C kao centar nacrtate se kružnica koja prolazi kroz tačke A i B .
- Ugao α koji određuje ravan normalnih napona određuje se na osnovu ugla 2α ($2\theta_p$)
- Ugao β koji određuje ravan maksimalnih tangencijalnih napona određuje se na osnovu ugla 2β ($2\theta_s$)

Naprezanje u dva pravca

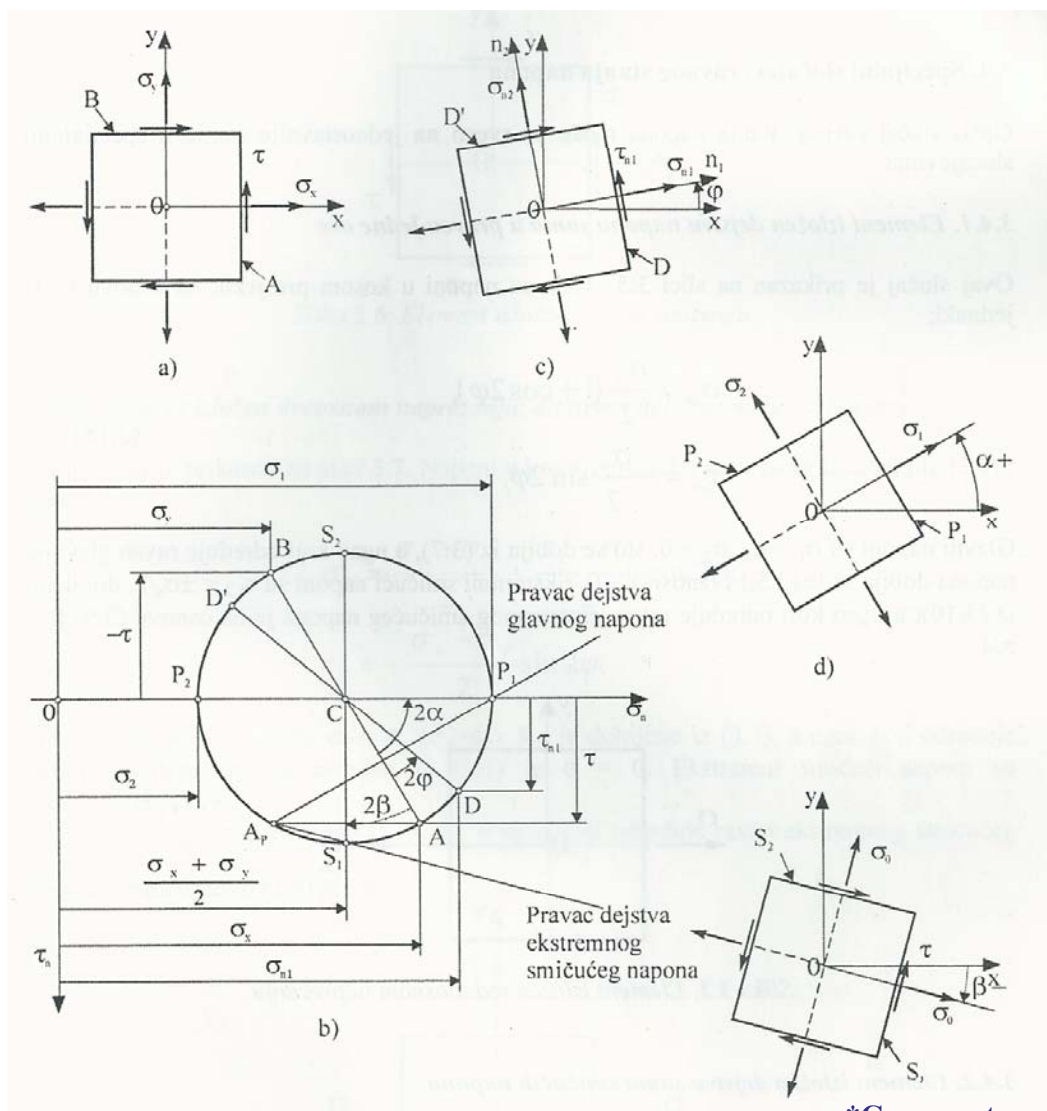
Mohr-ov (Mor) krug napona – konstrukcija



JM Gere, BJ Goodno, *Mechanics of Materials*, Cengage Learning, Seventh Edition, 2009.

Naprezanje u dva pravca

Mohr-ov (Mor) krug napona – određivanje napona za proizvoljnu ravan

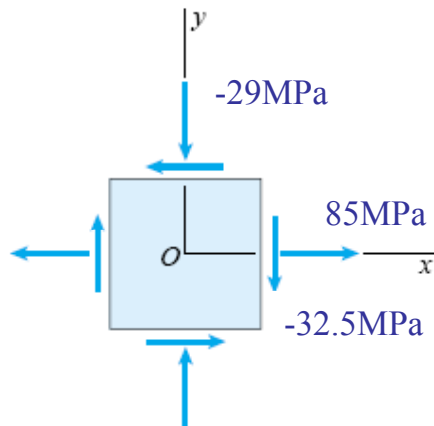


*Grupa autora, *Elastostatika I*, Tehnički fakultet, Bihać, 2003

Naprezanje u dva pravca

Primjer 3.1: Element je izložen naponima kao na slici: $\sigma_x=85\text{MPa}$, $\sigma_y=-29\text{MPa}$, $\tau_{xy}=-32.5\text{MPa}$.

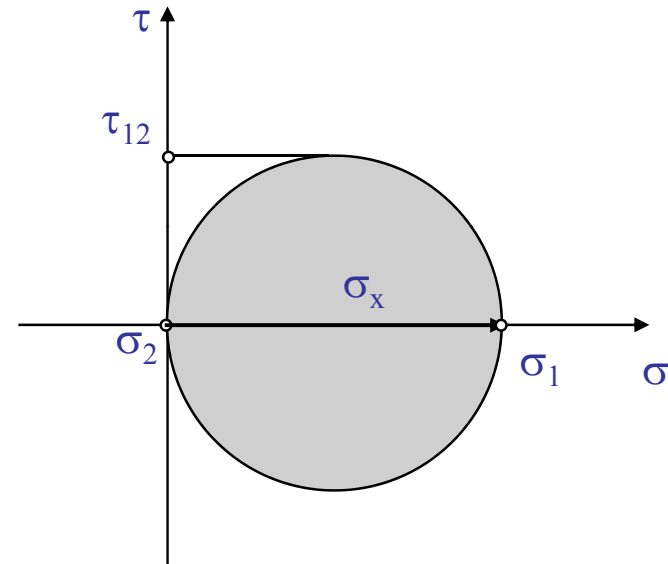
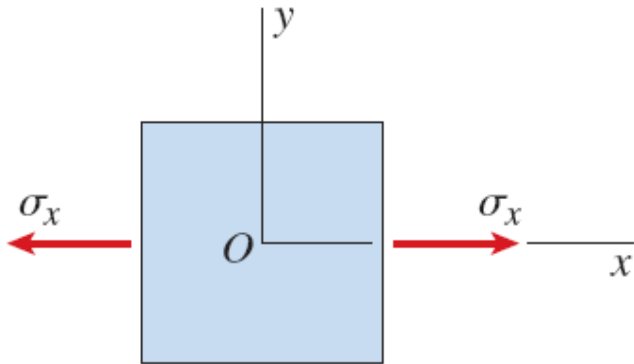
- Odrediti glavne napone i prikaži na skici elementa napona
- Odrediti maksimalni tangencijalni napon i pokaži na elementu napona
- rezultate pod a) i b) potvrdi konstrukcijom *Mohr*-ovog kruga napona



Naprezanje u dva pravca

Specijalni slučajevi dvoosnog naponskog stanja

Aksijalno naprezanje



$$\sigma_{x_1} = \frac{\sigma_x + \sigma_y}{2} + \frac{\sigma_x - \sigma_y}{2} \cos(2\theta) + \tau_{xy} \sin(2\theta)$$
$$\tau_{x_1y_1} = -\frac{\sigma_x - \sigma_y}{2} \sin(2\theta) + \tau_{xy} \cos(2\theta)$$

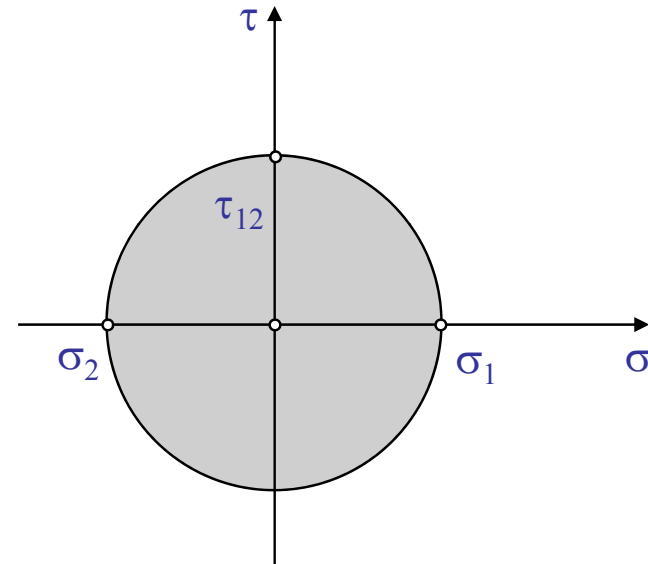
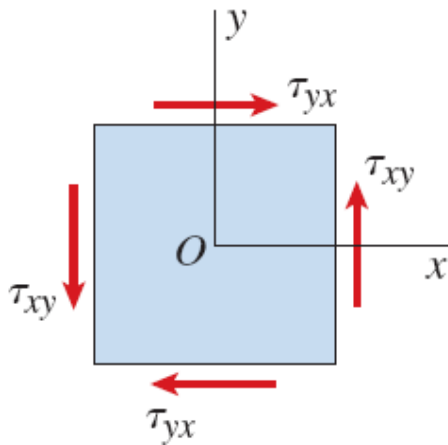


$$\sigma_{x_1} = \frac{\sigma_x}{2} (1 + \cos(2\theta))$$
$$\tau_{x_1y_1} = -\frac{\sigma_x}{2} \sin(2\theta)$$

Naprezanje u dva pravca

Specijalni slučajevi dvoosnog naponskog stanja

Čisto smicanje (bez normalnih napona)



$$\sigma_{x_1} = \frac{\sigma_x + \sigma_y}{2} + \frac{\sigma_x - \sigma_y}{2} \cos(2\theta) + \tau_{xy} \sin(2\theta)$$
$$\tau_{x_1 y_1} = -\frac{\sigma_x - \sigma_y}{2} \sin(2\theta) + \tau_{xy} \cos(2\theta)$$



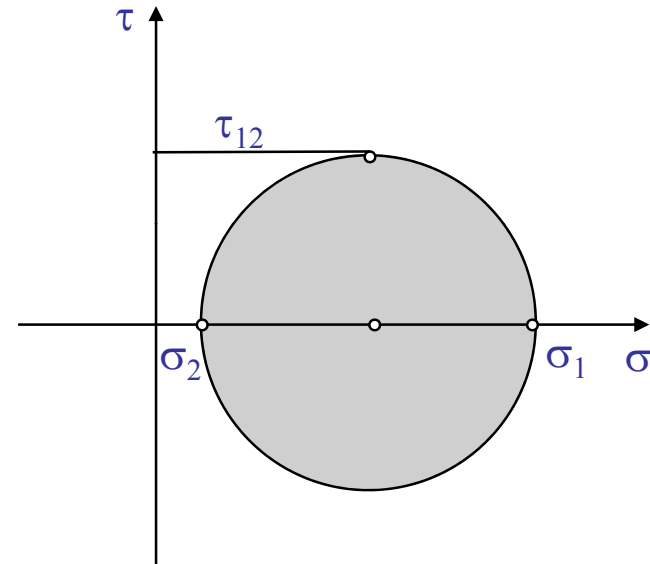
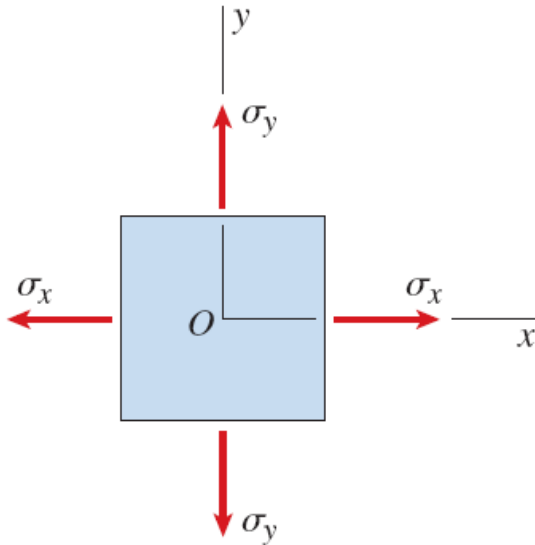
$$\sigma_{x_1} = \tau_{xy} \sin(2\theta)$$

$$\tau_{x_1 y_1} = \tau_{xy} \cos(2\theta)$$

Naprezanje u dva pravca

Specijalni slučajevi dvoosnog naponskog stanja

Dvoosno naprezanje, bez tangencijalnih napona



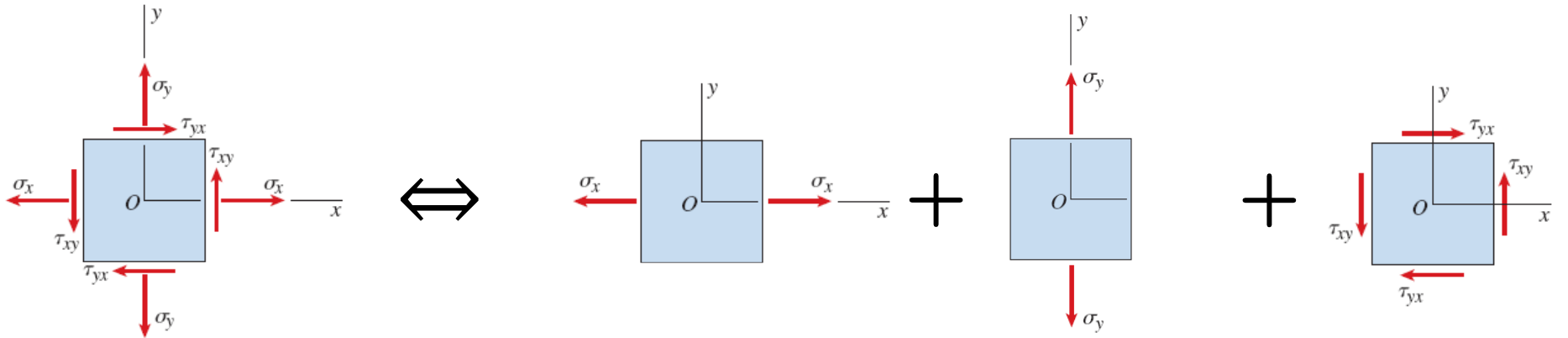
$$\sigma_{x_1} = \frac{\sigma_x + \sigma_y}{2} + \frac{\sigma_x - \sigma_y}{2} \cos(2\theta) + \tau_{xy} \sin(2\theta)$$
$$\tau_{x_1y_1} = -\frac{\sigma_x - \sigma_y}{2} \sin(2\theta) + \tau_{xy} \cos(2\theta)$$



$$\sigma_{x_1} = \frac{\sigma_x + \sigma_y}{2} + \frac{\sigma_x - \sigma_y}{2} \cos(2\theta)$$
$$\tau_{x_1y_1} = -\frac{\sigma_x - \sigma_y}{2} \sin(2\theta)$$

Naprezanje u dva pravca

Hooke-ov zakon za ravno stanje napona



$$\varepsilon_x = \frac{\sigma_x}{E}$$

$$\varepsilon_y = -\frac{\sigma_x}{E}$$

$$\varepsilon_x = -\frac{\sigma_y}{E}$$

$$\varepsilon_y = \frac{\sigma_y}{E}$$

$$\gamma_{xy} = \gamma_{yx} = \gamma = \frac{\tau}{G}$$

$$G = \frac{E}{2(1+\nu)}$$

$$\varepsilon_x = \frac{1}{E}(\sigma_x - \nu\sigma_y)$$

$$\varepsilon_y = \frac{1}{E}(\sigma_y - \nu\sigma_x)$$

+ utjecaj temperature

$$\varepsilon_x = \frac{1}{E}(\sigma_x - \nu\sigma_y) + \alpha\Delta T$$

$$\varepsilon_y = \frac{1}{E}(\sigma_y - \nu\sigma_x) + \alpha\Delta T$$

(3.17)

Naprezanje u dva pravca

Hooke-ov zakon za ravno stanje napona

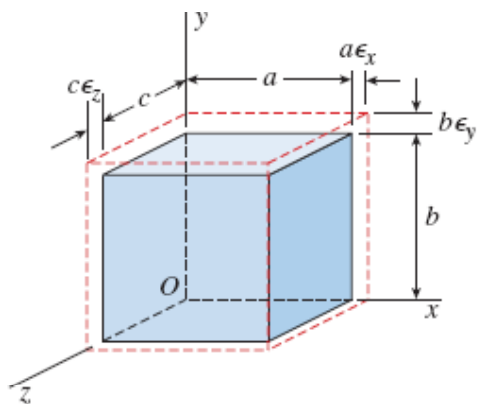
$$\begin{aligned} \varepsilon_x &= \frac{1}{E}(\sigma_x - \nu\sigma_y) \\ \varepsilon_y &= \frac{1}{E}(\sigma_y - \nu\sigma_x) \end{aligned} \quad + \quad \text{utjecaj temperature} \quad \begin{aligned} \varepsilon_x &= \frac{1}{E}(\sigma_x - \nu\sigma_y) + \alpha\Delta T \\ \varepsilon_y &= \frac{1}{E}(\sigma_y - \nu\sigma_x) + \alpha\Delta T \end{aligned} \quad (3.17)$$

$$\begin{aligned} \sigma_x &= \frac{E}{1-\nu^2}(\varepsilon_x + \nu\varepsilon_y) \\ \sigma_y &= \frac{E}{1-\nu^2}(\varepsilon_y + \nu\varepsilon_x) \end{aligned} \quad + \quad \text{utjecaj temperature} \quad \begin{aligned} \sigma_x &= \frac{E}{1-\nu^2}(\varepsilon_x + \nu\varepsilon_y) - \frac{E\alpha}{1-\nu}\Delta T \\ \sigma_y &= \frac{E}{1-\nu^2}(\varepsilon_y + \nu\varepsilon_x) - \frac{E\alpha}{1-\nu}\Delta T \end{aligned} \quad (3.18)$$

Naprezanje u dva pravca

Promjena zapremine i deformacioni rad

Dvoosno naprezanje, bez tangencijalnih napona



$$V_0 = abc$$

$$V_1 = (a + a\varepsilon_x)(b + b\varepsilon_y)(c + c\varepsilon_z) = abc(1 + \varepsilon_x)(1 + \varepsilon_y)(1 + \varepsilon_z)$$

$$V_1 = V_0(1 + \varepsilon_x)(1 + \varepsilon_y)(1 + \varepsilon_z)$$

$$V_1 \approx V_0(1 + \varepsilon_x + \varepsilon_y + \varepsilon_z)$$

$$\Delta V = V_1 - V_0 \approx V_0(\varepsilon_x + \varepsilon_y + \varepsilon_z)$$

Specifična promjena zapremine (dilatacija):
$$e = \frac{\Delta V}{V_0} = \varepsilon_x + \varepsilon_y + \varepsilon_z = \frac{1 - 2\nu}{E}(\sigma_x + \sigma_y)$$

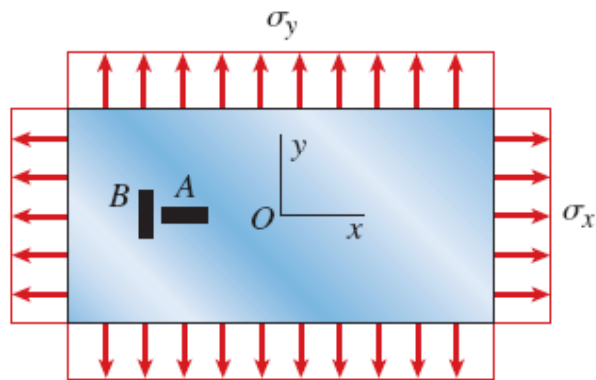
Deformacioni rad

$$W = \frac{1}{2}(\sigma_x \varepsilon_x + \sigma_y \varepsilon_y + \tau_{xy} \gamma_{xy})$$

$$W = \frac{1}{2E}(\sigma_x^2 + \sigma_y^2 - 2\nu\sigma_x\sigma_y) + \frac{\tau_{xy}^2}{2G}$$

Naprezanje u dva pravca

Primjer 3.2: Pravougaona čelična ploča debljine $t=6$ mm napregnuta je na ravnomjerne napone σ_x i σ_y , kao na slici. Mjerne trake A i B, koje su postavljene u pravcima x i y su postavljene na ploču. Ako su čitanja mjernih traka $\varepsilon_x=0.001$ (izduženje) i $\varepsilon_y=0.0007$ (skraćenje) izračunati napone σ_x i σ_y , te promjenu debljine ploče.
Podaci: $E=200\text{GPa}$.



Primjeri 3.1-3.14 (str. 74-88), Grupa autora, *Elastostatika I*, Tehnički fakultet, Bihać, 2003.
